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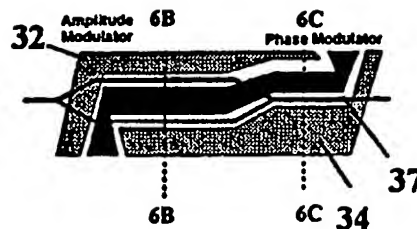
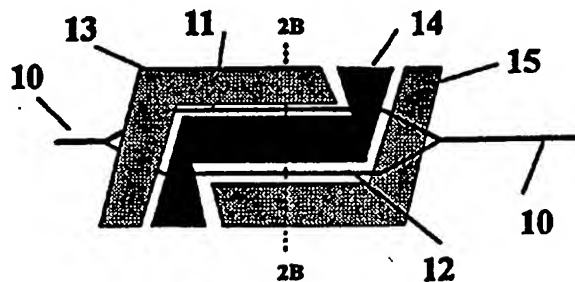
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(54) Title: **INTEGRATED OPTICAL MODULATORS**

(57) Abstract

An integrated optical modulator of the Mach-Zehnder type has a waveguide which, for part of its length, is divided into two waveguide sections (11, 12) arranged logically in parallel. Incoming light is divided to pass along the two sections (11, 12) and is then recombined before leaving the modulator. Each waveguide section has a pair of electrodes (13, 14) and (14, 15) associated therewith to generate an electric field through which the respective waveguide section passes, though there may be a single electrode (14) between the two waveguide sections (11, 12) to serve as one electrode of each pair, with the other electrode of each pair commoned. The physical arrangement of one waveguide section (11) and its associated electrodes (13, 14) is different from that of the other waveguide section (12) and its associated electrodes (14, 15), such that the electric fields to which light propagated along the two waveguide sections (11, 12) are respectively subjected are different when a single driving voltage is applied to the electrodes (13, 14, 15) associated with the waveguide sections. In an alternative arrangement there is provided an amplitude modulator (30) followed by a phase modulator (31).



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## INTEGRATED OPTICAL MODULATORS

This invention relates to integrated optical modulators, and also to methods of operating integrated optical modulators.

5 In the telecommunications industries, there is a demand for ever-increasing rates of data transmission. Optical communication networks are being used on an increasing scale on account of their ability to carry much higher data rates than electrical links, and various improvements are constantly being developed to  
10 allow optical data links to handle higher and higher data transmission rates. Unfortunately, the higher the data transmission rate, the shorter the maximum possible length of a data link, before regeneration of the data signal is required.

15 Currently, terrestrial telecommunications networks are being designed with a data rate of 2.5 Gb/s over 400 km, and 10 Gb/s over 100 to 150 km. Recently, there has been the introduction of optical amplifier components such as erbium-doped fibre amplifiers.  
20 These have allowed system designers to extend the physical length of an optical link before electrical regeneration is necessary.

Generally, the limiting factor for the length of a link is chromatic dispersion, which occurs because a  
25 transmitter has a real optical linewidth and the refractive index of a fibre varies, dependent upon wavelength. The optical fibres along which the data is transmitted have already been deployed extensively and so the system constraints are transferred into the transmitter design. For a given transmitter, the  
30 optical linewidth is determined by two factors, these being the inherent linewidth at DC and the broadening of the linewidth introduced by modulation. The latter factor is referred to as static chirp. In addition,

individual components may introduce a shift to the centre-frequency of the optical linewidth; this effect is usually referred to as dynamic chirp.

5 The modulation of an optical signal results in optical harmonics of the modulation frequency about the carrier frequency. If this modulated light is passed through a length of fibre which exhibits chromatic dispersion (that is, the fibre refractive index varies with wavelength), the phase of the light at the distal  
10 end of a fibre varies as a function of its frequency. Detection of received light causes mixing of the various frequency components, but as these will have differing phases, the mixing will result in the amplitude of the detected signal being changed on  
15 account of the linewidth of the transmitted signal.

As a result of static and dynamic chirp, there is introduced into an optically modulated and transmitted signal a pulse width change and an amplitude shift. In the case of the former, higher frequencies are reduced  
20 in amplitude and at some combinations of link length, dispersion and frequency, the signal to be detected can be nulled completely. In the case of the latter, positive dynamic chirp will broaden the width of a pulse propagating down a fibre and negative dynamic  
25 chirp will narrow the pulse. Either of these effects, if sufficiently large, will render a modulated signal undetectable.

With increasing speeds of transmission, it is important that a transmitter can achieve a defined and  
30 reproducible level of dynamic chirp. In order to maximise the repeater spacing, transmitters are being specified with a single value of dynamic chirp, with a specified tolerance. There is thus a demand for a modulator able to introduce a specified level of  
35 dynamic chirp into a modulated signal.

According to one aspect of the present invention, there is provided an integrated optical modulator having an optical waveguide which, for part of its length, is divided into two waveguide sections arranged logically in parallel whereby incoming light is divided into the waveguide sections and is then recombined after passing therealong, and a pair of electrodes for each waveguide section and arranged to generate an electric field through which the respective waveguide section extends, the physical arrangement of one waveguide section and its associated pair of electrodes differing from that of the other waveguide section and its pair of electrodes such that the electric fields to which light propagated along the two waveguide sections are subjected are different when the pairs of electrodes are driven with substantially the same voltage.

The term "logically in parallel", as used herein is intended to refer to the logical arrangement of the waveguide sections (i.e. not in series) rather than their physical arrangement. Thus, the waveguide sections may be linear and physically parallel, but other physical arrangements of the waveguide sections are equally possible.

In the present invention, the waveguide sections and the associated electrodes of a modulator have physically differing configurations in order to introduce an imbalance between the two arms of the modulator. This is achieved by dividing an optical signal to pass along the two sections and subjecting the divided signal to different electric fields, so giving a different phase shift in the two arms. Consequently, upon recombination of the optical signals after passing along the waveguide sections, the resultant modulated signal will display chirp, the

value of which will be dependent upon the chosen physical arrangement.

5 A typical integrated optical modulator is arranged as a Mach-Zehnder modulator having, for each waveguide section, a pair of electrodes between which there is defined a gap along which extends the associated waveguide section. The waveguide itself usually is formed in a substrate by a doping technique well known in the integrated circuit art. Equally, the formation of electrodes on that substrate is also well known in this art.

10 In a typical modulator as just described, there may be a single electrode between the two waveguide sections, which single electrode serves as one of the electrodes for each of the two electrode pairs. If the other electrodes of each electrode pair are connected together, a single drive voltage may be applied across the single electrode and said other electrodes, and yet the component will still produce a defined level of chirp. This may be contrasted with other designs of component intended to produce defined levels of chirp, where separate drive sources have to be provided for each arm of an interferometer, in order to introduce a relative phase shift between the two arms.

25 In one possible form of the present invention, the arrangement of the pair of electrodes associated with one waveguide section differs from the arrangement of the electrodes of the other waveguide section. For example, the gap between the two electrodes of one pair may be different from the gap between the electrodes of the other pair, whereby different electric fields are generated between the respective pairs of electrodes, for a common driving voltage. Alternatively, the arrangement of the pairs of the electrodes and the gaps therebetween may be essentially the same, but the disposition of each waveguide section with respect to

its associated gap may be different, for the two waveguide sections. In this case, one waveguide section may be offset laterally with respect to its associated electrodes, whereby that waveguide section will lie in a marginal region of the electric field between the electrodes, whereas the other waveguide section may be disposed substantially centrally with respect to the gap between its associated electrodes. Yet another possibility is to have the optical mode sizes (that is, in effect the cross-sectional areas) of the two waveguide sections different from each other.

A further possibility is to have the physical length of one waveguide section subjected to the electric field between its associated electrodes different from the physical length of the other waveguide section subjected to the electric field between its associated electrodes. This can be achieved either by providing electrodes defining gaps of different lengths, for the two waveguide sections, or by changing the physical length of the waveguide section lying within the gap between the respective electrodes.

In all of the above cases, the two waveguide sections and the electrodes are arranged as a Mach-Zehnder interferometer, to perform amplitude modulation on an incoming signal. The incoming light is divided into the two waveguide sections and then is subjected to a phase shift consequent upon the electric field through which the waveguide sections pass, which fields are generated by the electrodes associated with the respective sections. Then, on recombining the light, the two light portions will interfere to produce fringes resulting in a modulated optical signal. By adopting the measures defined in this invention, the precise nature of that interference will be affected,

so resulting in a controlled degree of chirp, for a given modulator.

According to a second aspect of the present invention, there is provided an integrated optical modulator having an optical waveguide along which incoming light is propagated, the waveguide being divided into a pair of logically in parallel waveguide sections into both of which incoming light is divided and is then recombined after passing therealong, a pair of electrodes for each waveguide section and arranged to generate an electric field through which the respective waveguide section extends whereby the waveguide sections form part of an amplitude modulator, and a part of the length of the undivided waveguide passing between a pair of electrodes arranged to generate an electric field therebetween, so as to form a phase modulator for said part of the undivided waveguide.

In this form of the invention, the chirp is controlled by providing a conventional Mach-Zehnder interferometer type of amplitude modulator, resulting in amplitude modulation of the light passing through the component, but the light is also subjected to phase modulation. This phase modulation may be performed either before or after the amplitude modulation, by subjecting the light passing along the waveguide to an electric field. That electric field may be generated by a pair of electrodes, which may be common with one of the pairs of electrodes used in the amplitude modulator.

According to a further aspect of the present invention, there is provided a method of controlling the chirp of an integrated optical modulator having an optical waveguide which, for part of its length, is divided into two waveguide sections arranged logically in parallel so that incoming light is divided into the



5 waveguide sections and then is recombined after passing therealong, each waveguide section having a respective pair of electrodes associated therewith to generate an electric field through which the respective waveguide section extends, in which method both pairs of electrodes are driven with the substantially same voltage but the respective fields to which the two waveguide sections are subjected are different.

10 According to yet another aspect of the present invention, there is provided a method of controlling the chirp of an integrated optical modulator having an optical waveguide along which incoming light is propagated, the waveguide being divided into a two waveguide sections arranged logically in parallel and  
15 there being a pair of electrodes for each waveguide section, in which method: incoming light is divided into both waveguide sections and is then recombined after passing therealong; an electric field is generated between each pair of electrodes so that the  
20 light is subject to amplitude modulation upon being recombined; and the light passing through the device is subjected to phase modulation by generating an electric field between two electrodes disposed in the region of an undivided part of the waveguide.

25 By way of example only, certain specific embodiments of modulator constructed and arranged in accordance with the present invention will now be described in detail, reference being made to the accompanying drawings, in which:-

30 Figures 1A and 1B diagrammatically illustrate a known form of Mach-Zehnder modulator in plan and cross-section, the section line 1B-1B being marked on Figure 1A;

35 Figures 2A and 2B diagrammatically illustrate a first embodiment of modulator of the present invention;

Figures 3A and 3B, and 4A and 4B are similar to Figures 2A and 2B, but of second and third embodiments of modulator of the present invention;

5       Figures 5A, 5B and 5C diagrammatically illustrate a plan view and two sectional views of a fourth embodiment modulator of the present invention; and

Figures 6A, 6B and 6C are similar to Figures 5A, 5B and 5C but of a fifth embodiment of modulator of the present invention.

10       Referring initially to Figures 1A and 1B, there is shown diagrammatically a Mach-Zehnder type of integrated optical amplitude modulator fabricated using conventional integrated circuit techniques but configured to allow the propagation of light along  
15       waveguides formed in a substrate typically of lithium niobate. The waveguide 10 is divided into two waveguide sections 11 and 12 arranged in parallel, such that an incoming light wave is split into the two waveguide sections, and then recombined so as to cause  
20       interference fringes.

On the substrate, there are formed electrodes 13, 14 and 15 arranged in two pairs with respective gaps 16 and 17 therebetween, the central electrode 14 being common to each of the two pairs. The outer two  
25       electrodes 13 and 15 are electrically connected together, in order that the same electric field will exist between the two pairs of electrodes, as shown in Figure 1B, for a single driving signal applied across the central electrode 14 and the common outer  
30       electrodes 13 and 15.

The arrangement illustrated in Figures 1A and 1B is essentially symmetrical; in order that each waveguide section 11 and 12 is subjected to the same electric field, when the same driving voltage is  
35       applied to the electrodes. Such an arrangement gives rise to zero dynamic chirp, unless only one electrode

pair is driven, in which case there will be  $\pm 1$  chirp. With this arrangement, no other chirp values can be obtained.

5 In the following description of specific embodiments of the present invention, components which are essentially the same as those described above with reference to Figures 1A and 1B are given like reference characters.

10 Figures 2A and 2B show a first embodiment of the present invention, wherein the physical arrangement determines the chirp of the resultant modulated waveform, when a single driving voltage is applied across electrode 14 and common electrodes 13 and 15, associated with the two waveguide sections 11 and 12.  
15 This is obtained by imbalanced modulation, by providing an enlarged gap 20 between electrodes 14 and 15, as compared to the gap 16 between electrodes 13 and 14, this gap 16 being comparable to that of the known arrangement of Figures 1A and 1B. The enlarged gap  
20 between electrodes 14 and 15 gives rise to an electrical field of a different configuration as compared to the field generated by electrodes 13 and 14. Thus, the two waveguide sections 11 and 12 are subject to different electric fields and light passing  
25 along the two waveguide sections 11 and 12 undergo different phase shifts, resulting in non-zero, non-unity chirp, as compared to the known arrangement of Figures 1A and 1B. The chirp is however defined, fixed and repeatable, for that modulator.

30 Figures 3A and 3B show an alternative modulator arrangement, where the electrodes 13, 14 and 15, and the gaps 16 and 17 therebetween are as shown in Figure 1B. The waveguide section 11 is disposed with respect to its gap 16 as in Figure 1B, but waveguide section 22  
35 is displaced laterally of the gap 17. In this way, the waveguide section 22 lies in a different electric field

as compared to waveguide section 11, when a single driving voltage is applied across electrode 14 and common electrodes 13 and 15. Consequently, a defined non-zero, non-unity chirp will be obtained, as with the arrangement of Figures 2A and 2B.

In Figures 4A and 4B, the optical waveguide mode sizes (that is, the cross-sectional areas) of the two waveguide sections 25 and 26 are different, though the configuration of the electrodes 13, 14 and 15 and the gaps 16 and 17 are the same as in the modulator of Figures 1A and 1B. Imbalanced modulation is thus obtained, since the overlap integral between the electrical and optical fields is different for the two waveguide sections.

Figures 5A, 5B and 5C show an arrangement where there is an imbalance in the physical length of the waveguide sections 27 and 28 subjected to the electric fields between the electrodes 13,14 and 14,15. This is achieved by having waveguide section 27 extending along the entire length of the gap 16 between the associated electrodes, but having waveguide section 28 extending along only part of the length of gap 17. The waveguide section 28 is then stepped laterally as shown in Figures 5A and 5C, so that the remaining part of the length of that section lies outside the electric field, or in only a weak field.

Figures 6A, 6B and 6C show an alternative modulator arrangement where there is provided an amplitude modulator 30 essentially of the same construction as shown in Figures 1A and 1B, but followed by a phase modulator 31. The electrodes 32, 33 and 34 are configured to define two gaps 35 and 36 both of which are of non-linear form, whereby the undivided waveguide 37 extends along gap 36 between electrodes 33 and 34, for part of its length. This undivided waveguide 37 is thus subject to the electric

field between electrodes 33 and 34, as is waveguide section 39, in the amplitude modulator section of the overall modulator. Waveguide section 38 is subjected to the field between electrodes 32 and 33, as for a  
5 conventional amplitude modulator, as described with reference to Figures 1A and 1B. This arrangement will also result in non-zero, non-unity, fixed and repeatable chirp in the modulated signal.

## CLAIMS

1. An integrated optical modulator having an optical waveguide which, for part of its length, is divided into two waveguide sections arranged logically in parallel whereby incoming light is divided into the waveguide sections and is then recombined after passing therealong, a pair of electrodes for each waveguide section and arranged to generate an electric field through which the respective waveguide section extends, the physical arrangement of one waveguide section and its associated pair of electrodes differing from that of the other waveguide section and its pair of electrodes such that the electric fields to which light propagated along the two waveguide sections are subjected are different when the pairs of electrodes are driven with substantially the same voltage.
2. An integrated optical modulator as claimed in claim 1, wherein each pair of electrodes defines a gap therebetween and along which gap extends the associated waveguide section for at least a part of the length thereof.
3. An integrated optical modulator as claimed in claim 2, wherein the arrangement of the pair of electrodes associated with one waveguide section differs from the arrangement of the electrodes associated with the other waveguide section.
4. An integrated optical modulator as claimed in claim 3, wherein the gap between the two electrodes of one pair is different from the gap between the electrodes of the other pair whereby different electric fields lie between the respective pairs of electrodes, for a common driving voltage.
5. An integrated optical modulator as claimed in claim 2, wherein the arrangement of the pairs of electrodes and the gaps therebetween are essentially

the same, and the disposition of each waveguide section with respect to its associated gap is different for the two waveguide sections.

5 6. An integrated optical modulator as claimed in claim 5, wherein one waveguide section is offset laterally with respect to the gap between its associated electrodes, and the other waveguide section is disposed substantially centrally with respect to the gap between its associated electrodes.

10 7. An integrated optical modulator as claimed in claim 2, wherein the optical mode sizes of the two waveguide sections are different.

15 8. An integrated optical modulator as claimed in claim 2, wherein the physical length of one of the waveguide sections subjected to an electric field between its associated pair of electrodes is different from the physical length of the other waveguide section subjected to an electric field between its associated pair of electrodes.

20 9. An integrated optical modulator as claimed in claim 8, wherein the length of the gap between the electrodes associated with said one waveguide section is shorter than the length of the gap between the electrodes associated with the other waveguide section.

25 10. An integrated optical modulator as claimed in claim 8 or claim 9, wherein the physical lengths of the two waveguide sections are substantially the same but the physical length of one waveguide section extending within the electric field between its associated electrodes is different from that of the other waveguide section.

30 11. An integrated optical modulator as claimed in any of the preceding claims, wherein the waveguide and the electrodes are arranged as a Mach-Zehnder  
35 interferometer.

12. An integrated optical modulator having an optical waveguide along which incoming light is propagated, the waveguide being divided into a pair of logically in parallel waveguide sections into both of which incoming light is divided and is then recombined after passing therealong, a pair of electrodes for each waveguide section and arranged to generate an electric field through which the respective waveguide section extends whereby the waveguide sections form part of an amplitude modulator, and a part of the length of the undivided waveguide passing between a pair of electrodes arranged to generate an electric field therebetween, so as to form a phase modulator for said part of the undivided waveguide.

13. An integrated optical modulator as claimed in claim 12, wherein the electrodes which generate the electric field between which the undivided waveguide passes comprise one of the pairs of electrodes of the divided waveguide sections.

14. An integrated optical modulator as claim in any of the preceding claims, wherein one electrode of each said pair of electrodes is common to both pairs of electrodes.

15. An integrated optical modulator as claimed in claim 14, wherein the other electrode of one pair is electrically connected to the other electrode of the other pair.

16. A modulator system comprising an integrated optical modulator according to any of the preceding claims, a laser light source providing a fixed wavelength unmodulated light signal to the modulator, and driving means connected to the electrodes of the modulator and arranged to apply substantially the same modulating drive voltage to the pairs of electrodes associated with the two waveguide sections respectively.

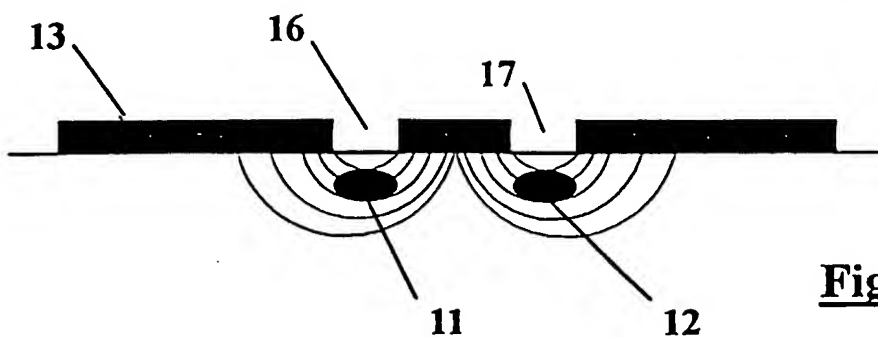
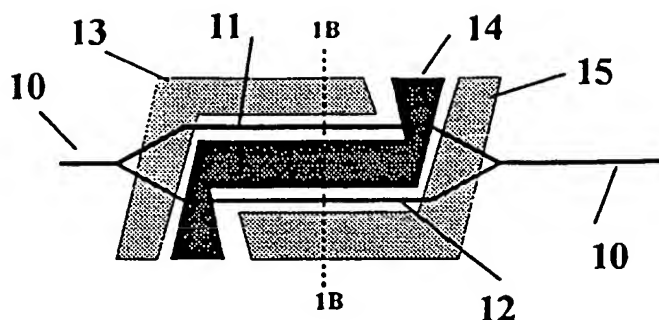


17. A modulator system as claimed in claim 16, wherein one electrode of each pair is common to both pairs of electrodes, the other electrodes of both pairs are connected together, and the driving means comprises a single drive source which applies a drive voltage across the one electrode and the connected-together other electrodes.

18. A method of controlling the chirp of an integrated optical modulator having an optical waveguide which, for part of its length, is divided into two waveguide sections arranged logically in parallel so that incoming light is divided into the waveguide sections and then is recombined after passing therealong, each waveguide section having a respective pair of electrodes associated therewith to generate an electric field through which the respective waveguide section extends, in which method both pairs of electrodes are driven with the substantially same voltage but the respective fields to which the two waveguide sections are subjected are different.

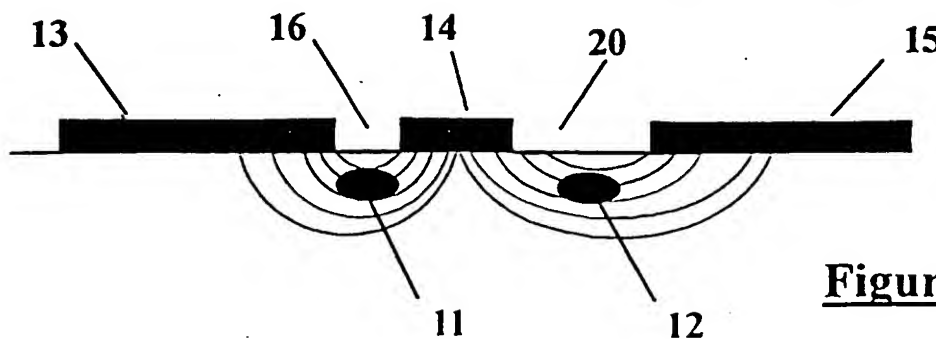
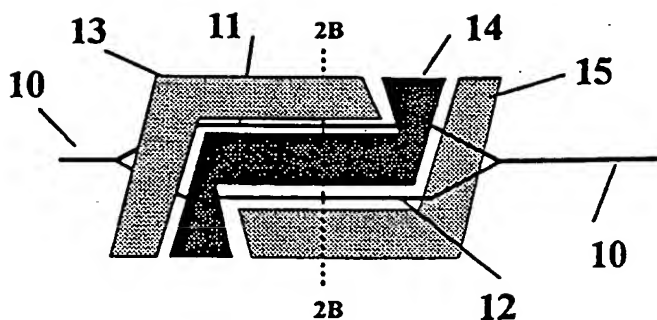
19. A method of controlling the chirp of an integrated optical modulator having an optical waveguide along which incoming light is propagated, the waveguide being divided into a two waveguide sections arranged logically in parallel and there being a pair of electrodes for each waveguide section, in which method: incoming light is divided into both waveguide sections and is then recombined after passing therealong; an electric field is generated between each pair of electrodes so that the light is subject to amplitude modulation upon being recombined; and the light passing through the device is subjected to phase modulation by generating an electric field between two electrodes disposed in the region of an undivided part of the waveguide.

**Figure 1A**



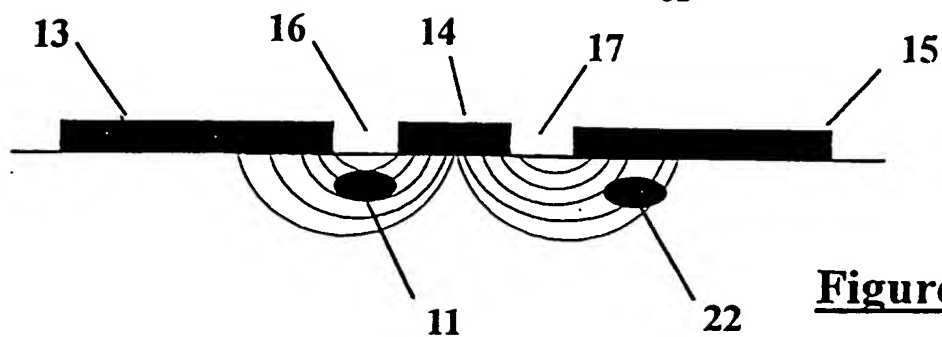
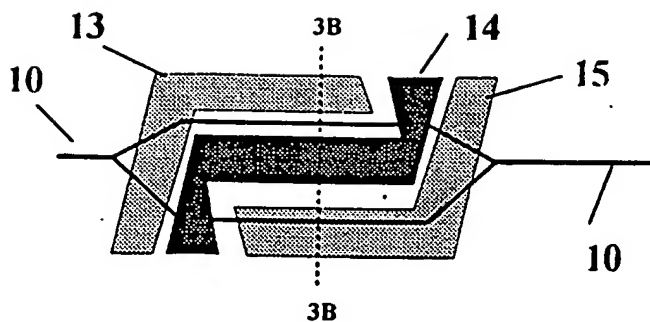
**Figure 1B**

**Figure 2A**



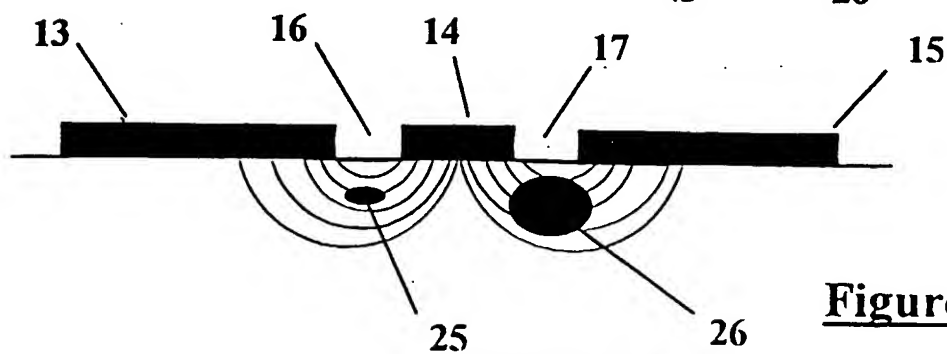
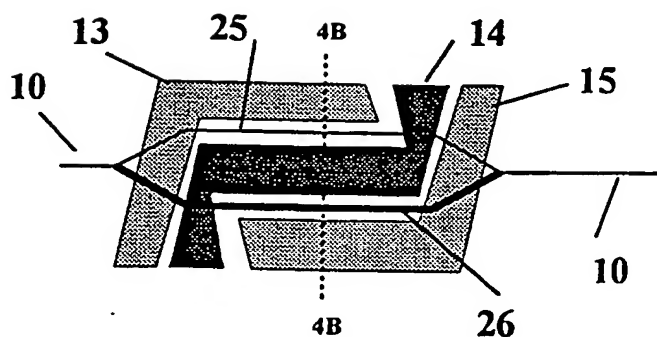
**Figure 2B**

**Figure 3A**



**Figure 3B**

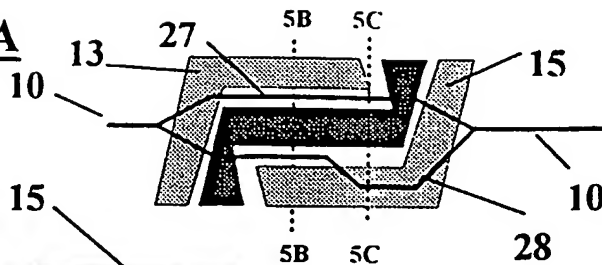
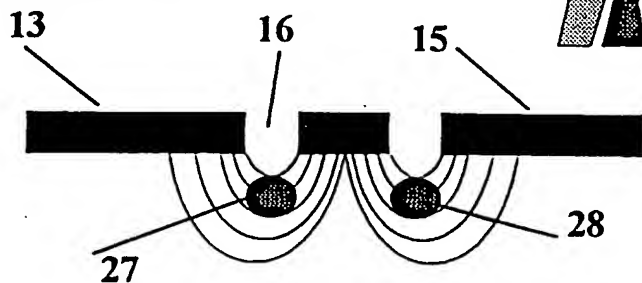
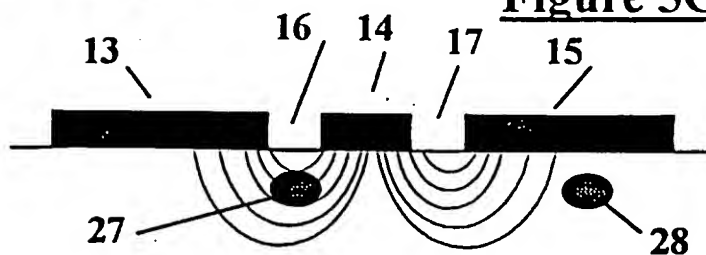
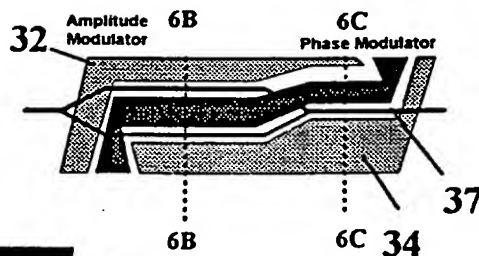
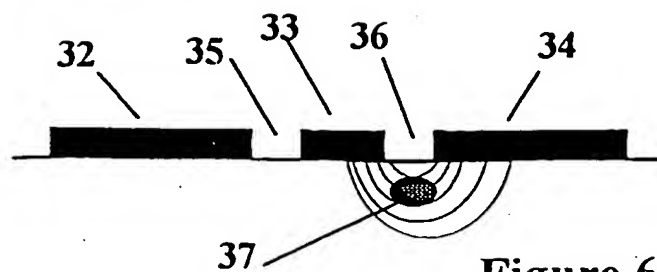
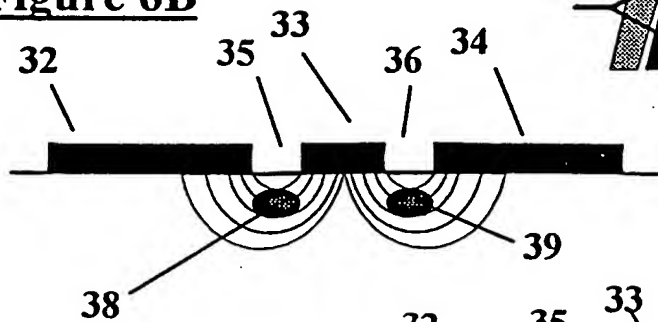
**Figure 4A**



**Figure 4B**

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Figure 5AFigure 5BFigure 5CFigure 6AFigure 6BFigure 6C

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